SSC-304 (SL-7-26)

SL-7 EXTREME STRESS DATA COLLECTION AND REDUCTION



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An Interagency Advisory Committee Dedicated to Improving the Structure of Ships

SR-1245

1981

This report is one of a group of Ship Structure Committee Reports which describe the SL-7 Instrumentation Program. This program, a jointly funded undertaking of Sea-Land Service, Inc., the American Bureau of Shipping and the Ship Structure Committee, represents an excellent example of cooperation between private industry, classification authority and government. The goal of the program is to advance understanding of the performance of ships' hull structures and the effectiveness of the analytical and experimental methods used in their design. While the experiments and analyses of the program are keyed to the SL-7 containership' and a considerable body of the data developed relates Specifically to that ship, the conclusions of the program will be completely general, and thus applicable to any surface ship structure.

The program includes measurement of hull stresses, accelerations and environmental and operating data on the S.S. Sea-Land McLean; development and installation of a microwave radar wavemeter for measuring the seaway encountered by the vessel, a wave tank model study and a theoretical hydrodynamic analysis which relate to the wave induced loads, a structural model study and a finite element structural analysis which relate to the structural reponse, and installation of long-term stress recorders on each of the eight vessels of the class. In addition, work is underway to develop the initial correlations of the results of the several program elements.

Results of each of the program elements are being made available through the National Technical Information Service, each identified by an SL-7 number and an AD- number. A list of all SL-7 reports available to date is included in the back of this report.

This report documents the installation of the long-term stress recorders and the method involved in selecting and converting the raw stress data to histograms. The reduction of a seven-year collection of these data are presented.

Rear Admiral, U.S. Coast Guard Chairman, Ship Structure Committee

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METRIC CONVERSION FACTORS

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CONTENTS

Page

I.	BACKGROUND	1
II.	FUNCTIONAL DESCRIPTION	1
III.	VESSEL DEPLOYMENT AND EQUIPMENT HISTORY	6
IV.	DATA PRESENTATION AND INTERPRETATION	8
۷.	DISCUSSION	36
VI.	SUMMARY	37
VII.	ACKNOWLEDGEMENT	37
	APPENDIX A - SCRATCH GAUGE INSTALLATION	38
	APPENDIX B - RECORDER CALIBRATION DATA	41
	APPENDIX C - HISTOGRAM COMPUTER LISTING	45
	APPENDIX D - DATA AVERAGES	47

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I. BACKGROUND

This seven-year data collection program has been conducted in three phases. The first three years of the program were conducted under Department of the Navy Contract N00024-73-C-514D. Serial No. SF35422306 Task 2022, SR215. The next two years were conducted under Coast Guard Contract D0T-CG-61712A. Report SSC-286(SL-7-25) covering the first five years was published by the Ship Structure Committee in 1979. The final two years of data collection was also sponsored by the Ship Structure Committee, Contract No. D0T-CG-844331-A. Project SR-1245-SL-7 "Extreme Stress Data Collection and Reduction." The present report collates data from the final two years with data previously reported, to provide a comprehensive summary of all the data.

Nine N.C.R.E. mechanical strain-gauge recorders were installed on the eight SL+7 high-speed containerships operated by Sea-Land Service, Inc. These vessels operated on both transatlantic and transpacific routes.

11. FUNCTIONAL DESCRIPTION

The purpose of this program was to obtain as much midship bending stress data from the SL-7's in the simplest and most direct manner possible. To meet this requirement, N.C.R.E. (Naval Construction Research Establishment) maximum-reading strain-gauge recorders and clock units (Figures 1 and 2) were obtained from Elcomatic Limited of Glasgow, Scotland. The units were installed at approximately midships in the starboard longitudinal box girder (tunnel) of all eight SL-7s (see Appendix A for installation details).

The N.C.R.E. strain gauge consists of contact points 10 inches apart and a mechanical linkage which provides a magnification of approximately 100:1 at the stylus. The stylus moves against a pressure-sensitive recording paper causing both positive and negative deflections to be indicated by a scratch mark (Figure 3). The paper is indexed about 0.1 inch every four hours. Once every sixth interval (i.e., every 24 hours) the index is 0.4 inches wide. Each vertical marking has a length which represents the maximum peak to maximum trough stress which has occurred during the four-hour period during which the stylus was at one place on the paper. For accurate data interpretation, it is important to remember the following characteristics of this system:

1. The record indicates the combined wave-induced and first-(or higher) mode vibratory stresses; there is no way to separate the various effects.

2. The maximum peak, and maximum trough stresses indicated on the record may not have occurred as part of the same cycle; i.e., they may have occurred at different times during the four hour record interval (Figure 4).

3. Slow "static" changes in the average stress caused by thermal effects, ballast changes, etc., will contribute to the total length of the scratch line. Appendix D of this report provides further information on these slow changes.

N.C.R.E. -maximum reading STRAIN GAUGE RECORDER

The analysis of wave-induced stresses imposed on the steel hull of a surface vessel involves the use of data relating to maximum bending moments applied to the hull girder. In the course of such analysis, scientific staff of the Naval Construction Research Establishment, Dunfermline, Scotland, adopted a method of recording maximum strain variations during specified time intervals by means of a maximum-reading strain gauge incorporating a strip chart.

Prototype quantities of the NCRE designed recorder were produced within the Establishment, subsequently evaluated and used as highly successful data acquisition instruments in the arduous environments experienced by Royal Navy warships at sea. To meet a demand for further models, it was decided by NCRE to permit a strain instrumentation company to manufacture the device commercially. Elcomatic Limited of Glasgow was chosen, and the NCRE recorder now is available as a standard Elcomatic product.



FIGURE 1

Gauge Action:

As shown in the sectional diagram below, the lever system is actuated by distortion of the structure under test and requires no external power supply. The instrument is bolted in position, bearing against the test surface on two sets of hardened conical studs. Any change in separation of bearing points is magnified by the lever system which drives the recording pen across the stationary reel of carbon-backed paper. Time related maximum strain records are obtained by forward movement of recording paper programmed by a precision battery-rewound clock and powered by a small motor also battery powered.



Prime function

Duration of Continuous unattended operation Magnification Factor

Resolution

Fully automatic recording of maximum strain. Three months depending on programme. Nominally 100-subject to precise calibration by a dial gauge reading to 0.0001 A strain change of 0.001 will produce a 1" pen deflection.

Temperature effects

Vibration

Chart loading

strain range of 0.0025. Uniform temperature changes of gauge and steel test structure produce no discernible pen movement. Tested by dynamic strains of double amplitude 0.0008 at frequencies 25 to 200 cycles per minute-no significant inaccuracy. Cassette.

FIGURE 2

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Analog Signal

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Scratch Gage

ILLUSTRATED EXAMPLE OF THE COMPARISON OF AN ANOLOG SIGNAL WITH THE SCRATCH GAGE

FIGURE 4

Prior to installations, each scratch gauge was calibrated utilizing a Bridgeport milling machine. The fixed collet and moveable table were used to generate strain. The table was moved in both tension and compression directions in increments of 0.001 inches, with a dial indicator used to measure the amount of displacement. A calibration table and plot for each instrument is provided in Appendix B of this report.

All of the scratch-gauge recorders and clock units have been removed from the vessels and returned to TES for storage. Each recorder was checked to insure that its calibration was still valid. No significant change in calibration was found.

III. VESSEL DEPLOYMENT AND EQUIPMENT HISTORY

The following section is a brief summary of each vessel's routing assignment from the time the scratch gauge(s) were installed until their removal. Included are comments concerning the operation of the equipment. The sequence is in the order in which the equipment was installed and placed in service.

The eight SL-7s have been utilized on either a transatlantic or transpacific route. Atlantic crossings involve some or all of the following ports: Port Elizabeth, N.J.; Portsmouth, VA; Bremerhaven, Germany; Rotterdam, Netherlands; and Algeciras, Spain. Those vessels assigned to Pacific duty followed a steady route that began in Seattle, Washington, with calls in turn at Long Beach, California; Oakland, California; Yokohama, Japan; Kobe, Japan; and Hong Kong.

For the first few years, the vessels operated at their designed speed of 33 knots. After the price of fuel quadrupled in the mid-seventies, the vessels' speed was reduced to 20-24 knots to conserve fuel and reduce operating costs.

1. SEA-LAND MCLEAN

This vessel became the test bed of the eight SL-7s. The hull and numerous components were heavily instrumented to investigate bending and torsional hull response. The data were published by the Ship Structure Committee as part of its SL-7 library. Two scratch gauges were installed October 7, 1972 (Serial No. BS72E0001 in the port tunnel, and Serial No. 026 in the starboard tunnel). Teledyne engineers rode this vessel for the winter months of 1972 to 1975 and were able to monitor the scratch gauges daily during this period. The <u>McLean</u> sailed the Atlantic until May 1975, when she transferred to the Pacific after a dry-docking at Newport News, Virginia.

In order to ascertain if the calibration curve for an installed unit had changed with time, the McLean port tunnel gauge was removed on October 18, 1975 and replaced with the spare unit (Serial No. BS73E0001). The removed unit was returned to TES and recalibrated. See Appendix B for the results of this test.

Both instruments performed well up to the time of their removal on September 14, 1980. One clock unit failed in May 1978, and one roll of tape from the port gauge was lost due to loss of stylus pressure in April-May 1979.

2. SEA-LAND GALLOWAY

Gauge unit Serial No. BS73A007 was installed in the starboard tunnel on March 10, 1973. A problem with excessive moisture condensation in the tunnels during the winter months was solved by placing a plexiglass enclosure around each unit and using a 40-watt light bulb as a heat source. Both the <u>Galloway</u> and <u>McLean</u> were retrofitted with this arrangement, and it was included for all subsequent installations. The <u>Galloway</u> started in Atlantic service, transferred to the Pacific in September 1973, and then returned to the Atlantic in December 1975.

Data output from the <u>Galloway</u> has not been up to a par with the other 'vessels. Numerous nagging problems encountered over the years include clock failures, broken wires, improper stylus pressure, loose screws, and a constant crew change.

3. SEA-LAND COMMERCE

Scratch-gauge Serial No. BS73A002 was installed on May 8, 1973 prior to the ship sailing for Pacific duty. The Commerce has remained in the Pacific ever since. The data from this ship have been good. Early problems included a defective drive motor and clock failure. Periodic clock and switch problems occurred, but did not cause any major interruptions of data collection. The unit was removed from service September 10, 1980.

4. SEA-LAND EXCHANGE

Scratch-gauge Serial No. BS73A004 was installed on May 13, 1973. The vessel stayed in Atlantic service until November 1973, when she transferred to, and remained in, the Pacific. With the exception of clock problems in 1975, the data received from this vessel have been excellent. The credit for this must go to the Chief Engineer, who took a personal interest in this project and provided on-board care for the unit.

Removal was on April 12, 1980 during a regular service call. The entire recorder drive chain of gears had stripped. It was also anticipated at that time that the SL-7s would be out of service by mid-summer because of their expected sale to the U.S. Government.

5. SEA-LAND TRADE

Scratch-Gauge Serial No. BS73A008 was installed on May 22, 1973. The vessel transferred immediately to Pacific Service and remained there. This system performed well until May, 1976, when the dynamic response data did not seem to match data from other Pacific vessels. In September, 1977 the unit was removed and Serial No. BS72E001 (the original McLean port gauge) was installed. The quality of the data returned to normal. The problem was found to be caused by the misalignment of the mechanical multiplier arm. With this exception, this unit produced excellent data, and credit must go to the two Chief Engineers who provided the on-board care. The unit was removed from service on September 25, 1980.

6. SEA-LAND FINANCE

Scratch-Gauge Serial No. BS73A005 was installed October 3, 1973 prior to her departure for the Pacific, where she remained. A broken mounting stud was repaired in June 1974 and a clock replaced in October 1979. The unit was removed September 28, 1980. This unit has produced good data during its entire service.

7. SEA-LAND MARKET

Scratch-Gauge Serial No. BS73A003 was installed on November 5, 1973. This vessel has remained in Atlantic service during her operational life. Clock problems were encountered during the first year, and switch problems during 1979. With these two exceptions, the unit has been satisfactory. The unit was removed from service on November 13, 1980.

8. SEA-LAND RESOURCE

Scratch-Gauge Serial No. BS73A006 was installed on December 13. 1973. This ship was originally assigned to the Pacific, but returned to Atlantic service late in 1974. This unit was plagued with problems during its entire service. Stylus problems occurred in 1974-1975 and again in 1979. Clock failures occurred in 1976-1977-1979 and early 1980. In addition, a number of data tapes were lost in the mail. The unit was removed October 30, 1980.

SUMMARY

Most of the systems have performed well. The battery-operated clock is the major weak link. Periodic routine maintenance is required to keep these systems at top performance. On-board care was reduced to changing tapes and batteries. Usually, the Chief Engineer of each vessel undertook this responsibility. He also annotated the tapes with the date and time periodically. In general, the cooperation was excellent throughout the entire program.

IV. DATA PRESENTATION AND INTERPRETATION

As previously stated, the data have been collected on rolls of pressure-sensitive paper. Each roll represents approximately three months' time and usually, at least, 2 rolls of tape are collected during each six-month visit to the vessel. In order to protect the data and facilitate analysis, each data roll was subsequently mounted on $8 \ 1/2 \ x \ 11''$ card stock with usually 3 strips of the roll mounted per sheet. This is approximately two weeks of real-time data.

The length of each data marking (scratch) has been measured to the nearest 0.02 inch and the results tabulated for each vessel over the seven data years of information collected. It is this data tabulation which supplies the basis for the histograms which are presented in the following pages. In order to present the data in a more useful form (i.e., psi of midships bending stress vs. number of occurrences) it was necessary to perform the following transformation: Since the scratch gauge is substantially linear, its calibration curve is approximated by a straight line, and this by the equation

$$y = Mx + B$$

where

y = stylus deflection in inches
X = null girder elongation in 10 inches
B = Slope of the calibration curve
around the point of interest

If we assume that the scratch gauge operates around the zero points; i.e., there is no constant stress and any offset due to loading is ignored, "B", the slope intercept, is zero.

Solving for X:

 $X = \frac{y}{M}$

Stress (psi) = (E, Young's Modulus for Steel) (Elongation in 1 inch)

$$\sigma = (30 \times 10^{6}) \left(\frac{y}{M} \times 10^{-1}\right),$$

$$\sigma = (3 \times 10^{6}) \frac{y}{M}$$

and

or

 σ psi = (3×10^6) (length of scratch line in inches) (slope of the best straight line approximation)

The lengths of the scratch lines have been tabulated. The slope of the calibration curve for each vessel has been derived from the calibration plots of Appendix B and is tabulated in Table I. Since the majority of the data points lie between a gauge deflection of +0.4 inches to -0.4 inches, the slope of the line was calculated between these two values. The stress value for each data interval, therefore, can be calculated from:

psi = (length of scratch line in inches) x (scale factor)

The scale factors have been calculated for each gauge and are presented in Table II. Thus, all the information to prepare histograms of stress levels versus the number of occurrences has been developed.

TABLE I

SLOPES OF CALIBRATION CURVES

TABLE II

DATA MULTIPLICATION SCALE FACTORS

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	Calibration	Slope		
Scratch Gauge	Curve	Value		
	(Fig.)			
			SCRATCH GAUGE	SCALE FACTOR
McLEAN PORT				
Original	B-1	87	MCLEAN PORT	
Recalibration	B-2	88	Original	3.448 x 10 ⁴
Spare (Replacement)	B-3	96	Spare (Replacement)	3.125×10^4
MCLEAN STBD	B-4	94	McLEAN STBD	3.191×10^4
GALLOWAY	B-5	91 [°]	GALLOWAY	3.297×10^4
COMMERCE	B-6	. 88	COMMERCE	3.409×10^4
EXCHANGE	B-7	91	EXCHANGE	3.297×10^4
TRADE (Original)	B-8	97	TRADE (Original)	3.093×10^4
(Replacement)	B-2	88	(Replacement)	3.409×10^4
FINANCE	B-9	99	FINANCE	3.030×10^4
MARKET	B-10	82	MARKET	3.659×10^4
RESOURCE	B-11	86	RESOURCE	3.488×10^4

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The histograms are arranged in the order of data years. One histogram is provided for each gauge for each year. (In data year five, 2 histograms are provided for the SEA-LAND TRADE as two gauges of different calibration factors were used).

Associated with each year are three additional plots. A summary plot of all Atlantic data, a summary plot of all Pacific data, and a final plot of all data collected within the year. Finally, three summary total histograms are included: A seven-year Atlantic summary, a sevenyear Pacific summary. and a summary of all data collected during the seven-year period. Thus, a total of 88 histograms are presented (Figures 5 through 92, inclusive).

To facilitate data presentation, the data have been divided into "Data Years" as follows:

Data Year (1)

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September 1972 to May 1, 1974

The first year has been broadened to include the early contractual period which started in September of 1972 rather than starting with May 1, 1973, primarily because only the MCLEAN and GALLOWAY had their installations in operation prior to the May 1, 1973 date. Data year seven has also been expanded to include the remaining months of 1980 prior to system removal.

<u>Data Year (2)</u> May 1, 1974 - May 1, 1975 <u>Data Year (3)</u> May 1, 1975 - May 1, 1976 <u>Data Year (4)</u> May 1, 1976 - May 1, 1977 <u>Data Year (5)</u> May 1, 1977 - May 1, 1978 <u>Data Year (6)</u> May 1, 1978 - May 1, 1979 <u>Data Year (7)</u> May 1, 1979 - Fall 1980

As part of this contract, it was desired to establish a correlation between the <u>McLean</u> scratch-gauge data and tape-recorded stress data from the longitudinal vertical bending stress transducers in operation during the first two winter seasons.

(Text continues on Page 34)





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The tape-recorded stress data from the MCLEAN was recorded at four-hour intervals. These intervals were identified by time and date, along with other notations. The scratch-gauge folders first had to be identified by the same time and date for correlation with the tape recorded data. The two arrays of stress readings were then input as data to a calculator regression analysis program with the following results:

> x inputs = LVB stress y inputs = Scratch gage stress n = 238 $\Sigma x = 1,413,966$ $\Sigma y = 1,059,543$ $\Sigma x^2 = 1.444668878$ E10 $\Sigma y^2 = 9,328,072,353$ $\Sigma xy = 1.10976861$ E10

From these quantities the following intermediate quantities were calculated:

$$S_{xx} = \Sigma x^{2} - \frac{(\Sigma x)^{2}}{n} = 6,046,269,246$$

$$S_{yy} = \Sigma y^{2} - \frac{(\Sigma y)^{2}}{n} = 4,611,133,838$$

$$S_{xy} = \Sigma xy - \frac{\Sigma x \cdot \Sigma y}{n} = 4,802,905,522$$

And from these intermediate quantities the following ensues:

$$r = \frac{Sxy}{\sqrt{Sxx} \cdot Syy} = 0.91$$

$$b = \frac{Sxy}{Sxx} = 0.79$$

$$a = \overline{y} - b\overline{x} = \frac{\Sigma y}{n} = \frac{b \cdot \Sigma x}{n} = -267$$

"r" is the correlation coefficient and can vary from -1 to +1. A correlation coefficient of +1 indicates a perfect direct correlation. An r of -1 indicates a perfect inverse correlation and an r of zero indicates a complete non-correlation.

The constants a and b are used in the linear regression equation:

y = a + bx

Thus. the equation which defines the scratch-gauge variable y in terms of the LVD transducer x is:

 $y = 0.79 \times -267$

Without using statistics. a theoretical relationship between the scratch gauge and LVB transducer can be established by determining the ratio of the distance of the two transducers from the neutral axis. The LVB transducer is mounted on the underside of the main deck. The scratch gauge is mounted four longitudinal stringers below the main deck.

Dimensions taken from the Midship Section Drawing of the ship are:

Total Depth = 19510 mm Scratch+GaugeLocation = 2440 mm below deck Neutral Axis = 10743 mm below deck

The Neutral Axis Dimension was provided by J. J. Henry personnel at the time of original strain gauge transducer installation in Holland.

In this case, the scratch gauge's moment arm as a proportion of the LVB transducer's moment arm is:

 $y = \frac{10743 - 2440}{10743} x$ y = 0.77 x

The LVB transducer was wired to record vertical bending only. The scratch gauge sees transverse and torsion stresses as well as vertical bending. It is difficult to state what effect these other stresses have on the scratch-gauge excursions. However, the correlation of the statistical calculations from experimental data and the simple distance calculation is quite close, and would indicate that stresses other than pure vertical bending have little effect on scratch-gauge recordings.

The analysis presented above demonstrates that the scratch gauge on the <u>McLean</u> measures the extreme stresses experienced with reasonable accuracy. The other seven ships have no such independent means of verifying scratch-gauge accuracy, but by similarity, analogy, and consistency of the data, the data have every appearance of validity. A static calibration of the entire <u>McLean</u> instrumentation system was conducted in Rotterdam on April 9-10, 1973. Full particulars are published in report number SSC 263 (SL-7-7). The scratch gauges were manually advanced for each load condition and their values compared with strain gauge values. The starboard gauge is in close agreement with the Longitudinal Vertical Bending Stress Strain Gauges. The port gauge also was in close agreement, with the exception of loading condition No. 1. The stress values obtained during this calibration were extremely low, varying from -1500 to +2700 psi. The changes in stress for each condition produced scratch-gauge deflections in the order of 0.02 inch or less, making accurate measurement difficult. However, the scratch-gauge values were within the expected range.

V. DISCUSSION

Over 53,000 measurable readings of midship bending stress have been tabulated and presented in histogram form in the preceeding section. Appendix C shows a sample of the computer card listing of all the data by ship, ocean, folder number and approximate date, with the number of occurrences at each stress level. The scratch-gauge recorders, operating continuously, have also recorded numerous 4-hour intervals where no noticeable change has occurred. These intervals include such periods as time spent alongside the dock, calm weather operation, dry docking and repair layups. The scratch-gauge recorder provides a continuous bending stress history of the vessel. If the individual reducing the data from the tapes is familiar with the vessel's route and he has a known starting point on the tape, it is possible to trace the ship's movement out of port to the next port, observe the change in stress caused by loading and unloading. and the return to sea. As the ship departs a port and returns to sea, a distinct stress is recorded as the ship picks up speed. This stress is more pronounced when the ship's sea speed is over 20 knots. Recordings have been made when the vessels have gone into and out of drydock, and the static change can be easily noted. In many cases, it averages approximately 3000 psi change.

There are possibly other correlations that could be derived from this simple device, but a detailed loading distribution and the ship's log entries would be required to separate them.

In reviewing the histograms, it becomes evident that very few stress events exceed 20 kpsi. The <u>McLean's</u> highest stress occurred on December 19, 1973. This author was aboard at the time operating the instrumentation system. The strain gages recorded a maximum peak-to-trough stress of 53,600 psi while the port scratch gauge read 37,950 psi and the starboard scratch gauge read 32,857 psi. The ship was hove-to at the time in a Force 12 sea condition with the sea on the bow. The <u>Galloway</u>, eastbound earlier, was in the same storm and had a reading of 29,700 psi. The winter season of 1973-1974 was a series of heavy storms in the Atlantic. The <u>Market</u> also had a reading of 39,528 psi in January 1974. To return to the <u>McLean</u> data, the high strain reading was the result of one wave cycle occurring very rapidly. The scratch gauge, due to its mechanical operation, may not have responded fast enough to have measured the total stress, yet the ratio is close (0.71 vs. 0.79) to the statistical relationship between the two transducers. On the SL-7 class of vessel, the ship may roll heavily and also have a corkscrew type of motion, yet the vertical bending recorded will be quite low. With the sea on the bow or stern and a low pitching motion, the vertical bending is considerably higher.

The McLean recorded high stress again in December 1977, enroute to Seattle in the Gulf of Alaska. This time the wind and sea were on the stern, approximately Force 9.

The <u>Galloway</u> has recorded a few high stresses during its operation, however, correlation of the ship's activity and location has not been possible. The "Mariners Weather Log" published by the Department of Commerce is a valuable tool, as ships report unusual weather conditions and log entries. For example, the Galloway reported a severe storm on September 27, 1979 but the scratch-gauge records indicate a maximum stress of only 9900 psi. At the time, she was in the North Sea approaching Bremerhaven.

The <u>Trade</u> reported 50-knot winds and 33-foot waves on September 27, 1979. Stress levels from the scratch gauge have three instances in the low 20 kpsi range. Again in December, 1979 the <u>Trade</u> experienced 29-30 kpsi stress from 60 knot winds and relatively low seas.

Severe sea and weather conditions contribute to high bending stress, but the effects can be sharply reduced by the Captain of the vessel if he can reduce speed and/or change course.

All of the original data and summaries developed for this report are available in the SL-7 data library maintained at the Waltham, Massachusetts facility of Teledyne Engineering Services.

VI. SUMMARY

This seven-year program has been very successful in amassing a wealth of quality data. It has allowed the collection of bending data over a total of fifty-six statistical ship-years of operation. The cooperation of both vessel and port personnel on both coasts has been excellent. The scratch-gauge recorders and clocks have been removed from the vessels. Most of the units are in full operating conditions, and are available for further use.

The opinions and conclusions presented in this paper are those of the author, and not necessarily those of the Ship Structure Committee nor the United States Coast Guard.

VII. ACKNOWLEDGEMENT

The data presented in this report could not have been collected without the interest and assistance of the crew of each SL-7. Particular thanks go to the Chief Engineer of each vessel, who provided the on-board attention these installations require. In addition, we thank the Sea-Land shore personnel who assisted in mailing the tapes and keeping us informed of vessel locations and problems.

APPENDIX A

SCRATCH-GAUGE INSTALLATION

1. GENERAL

The installation of a scratch-gauge recording system aboard an SL-7 involves the mounting and wiring of three major components; the gauge itself, the clock assembly and the protective enclosure. With the exception of the MCLEAN, all vessels have single recorder installations located at approximately Frame 186 in the starboard longitudinal box girder (tunnel). The McLEAN has installations in both the port and starboard tunnels. Figure A-1 shows the configuration of the SL-7 class containership and the location of the scratch gauge. Figure A-2 shows the physical relationship of the recorder location to the rest of the vessel. The installation is made on the second-from-the-deck outboard longitudinal girder either at Frame 186 1/4 or 186 3/4 depending upon local interference problems.

2. PREPARATION

At the installation site, all components are physically placed in position and clearances checked. To ensure a minimum of effect on the vessel structure, all components are bolted to 1/4 - 20 studs which are welded to the steel with a stud welding machine. The first task is to mark all stud locations: six for the recorder,* four for the clock assembly and eight for the enclosure assembly.

Once the stud locations are marked, each area is cleaned to bare metal with a hand-held grinder and a center punch used to mark the stud center. This ensures that when the stud is welded a clean and strong weld is achieved.

* Although only 2 studs are required to mount the recorder, three pairs i.e., six studs were installed to provide spares in case of stud failure during the operational life. One such failure has occurred and the quick movement of the recorder to a spare set of studs was accomplished with a minimum of data loss.

3. INSTALLATION (Ref. Fig. A-3)

The clock assembly, the clock and its mounted plate, is bolted to the studs on the side shell. Next, the recorder is positioned and tightly secured. It is very important that the recorder studs be tight to ensure that the conical bearing points of the instrument are making good contact with the longitudinal girder.

The connecting cable from the clock to the recorder is then positioned and connected. With batteries in the clock unit, the hands are physically turned to ensure that the recorder advances at the desired 4-hour increments. When operation is satisfactory, the plexiglass enclosure (Fig. A-4) is positioned and bolted in place. Clear RTV (Room Temperature Vulcanizing) silicone rubber is then put around all edges to make a nearly watertight seal around the enclosure.

The lamp unit on the enclosure is wired to a local service of 115 V, 60 Hz, Single Phase power to operate the 40-watt lamp in the top.

A final check of the recorder ensures free movement of the stylus arm, and proper marking pressure on the paper tape. The clock is set to GMT and the front door of the enclosure closed.

We have requested that the chief engineer mark the tape with the date at least once a week. Each roll of tape lasts approximately 3 months, at which time both the tape and clock batteries should be changed. Spare tape, batteries, and lamp are kept inside each enclosure.



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SCRATCH GAUGE ENCLOSURE FIGURE A- 4



LAMP

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4"PLEXIGLAS



APPENDIX B

TABLE B-1

Scratch-Gauge Calibrations

Stylus Deflection, inch

Structure Deflection inch	McLean Port (original)	McLean Port* (recal.)	McLean Port (10/18/75)	McLean Stbd	Galloway Stod	Commerce Stbd	Exchange Stod	Trade Stød	Finance Stbd	Market Stbd	Resource Stbd
0.010	0.85	0.95		0.874							
0.008	0.692	0.76		0.712					0.76 0.66	0.64 0.56	0.70 0.62
0.006	0.536	0.57	0.58 0.45	0.560	0.53 0.45	0.53 0.45	0.64 0.54	0.56 0.46	0.60 0.488	0.49 0.42	0.54 0.44
0.004	0.338	0.37	0.38 0.30	0.388	0.33 0.28	0.33 0.28	0.44 0.36	0.36 0.28	0.40 0.30	0.34 0.26	0.36 0.28
0.002	0.172	0.20	0.20 0.10	0.198	0.16 0.12	0.15 0.12	$\begin{array}{c} 0.18 \\ 0.10 \end{array}$	0.20 0.06	0.20 0.12	0.17 0.10	0.18 0.09
0.0 -0.001	0.0	0.0	0.0 -0.100	0.0	0.0 -0.072	0.0 -0.072	0.0 -0.08	0.0 -0.128	0.0 -0.10	0.0 -0.10	0.0 -0.08
-0.002	-0.176	-0.15	-0.20 -0.28	-0.170	-0.16 -0.30	-0.16 -0.30	-0.18 -0.26	-0.232 -0.252	-0.20 -0.24	-0.18 -0.26	-0.16 -0.24
-0.004	-0.350	-0.33	-0.37 -0.47	-0.378	-0.39 -0.48	-0.39 -0.48	-0.36 -0.46	-0.408 -0.50	-0.392 -0.48	-0.34 -0.41	-0.33 -0.40
-0.006	-0.540	-0.53	-0.55 -0.68	-0.558	-0.51	-0.51	-0.552 -0.64	-0.60	-0.58 -0.66	-0.48 -0.58	-0.48
-0.008 -0.009	-0.688 -0.768	-0.72		-0.716			-0.72				
-0.010 Figure	8-1	-0.91 8-2	B-3	B-4	B-5	B-6	B-7	B-8	B-9	B-10	8-11

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* Installed on TRADE September 1977.

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APPENDIX C

HISTOGRAM COMPUTER LISTING

To facilitate future use of the data presented in the histograms included in this report, all of the data have been inputted on computer cards. The data are listed by data folder. Each folder (approximately 2 weeks of data) has a header card that lists in order: the vessel name, ocean, folder number, date and data year. This card is followed by data cards that list the number of occurrences at each stress level for that folder.

This encoded data are the result of measuring the scratch length and calculating the eqivalent stress for each gage as described in Section IV, A sample of the listing is included as Figure C-1. The complete listing is available on request.



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APPENDIX D

DATA AVERAGES

As required by the contract for the final portion of the scratch-gauge project, the top and bottom of each four-hour scratch mark on the data tape was measured from a reference line. The numerical average of each scratch was then calculated. The purpose of this calculation was to determine if it was possible to read diurnal stress or other static changes from the scratch-gauge records.

The measurements made were encoded on computer punch cards. A listing of these is presented in this Appendix. Each folder of data consists of a header card listing the vessel, ocean, folder number, date and data year, followed by data cards with Bottom-Top readings in hundredths of an inch (reading horizontally).

Although all the data areshown in the listing, only one folder of each ship's scratch gauge data is plotted and included here.

Each data point represents the four-hour extreme stress experienced underway with the time in port excluded. Each plot is divided into an ocean crossing portion, and time spent between ports. with all data in correct time sequence.

With the exception of the <u>Market</u> and <u>Resource</u> plots, the average stress change compared to peak-to-trough maximum stress during ocean crossings is quite low. There is no evidence of diurnal stress on any of the plots. On the McLean and Galloway plots and all of the others to some extent, there is evidence of bias to one side. This is shown as a repeated lower or upper reading regardless of the length of the total scratch excursion. The only explanation that I can conceive is that while at sea these vessels present a large sail-area to the wind and tend to sail with a constant list. This phenomenon is also observed in the ships roll where the roll to the windward is much less and more constant than the opposite roll. In reviewing expanded oscillograph records of McLean Bending Stress Data, the same bias was observable.

The trim of these constant-draft vessels is important, and as a result the crew monitor the fuel consumption and ballast conditions, and adjust them as required a minimum of twice a day and more often as required. This constant trim keeping would result in the small change of average stress evidenced by the data.





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The SHIP DESIGN, RESPONSE, AND LOAD CRITERIA ADVISORY GROUP prepared the project prospectus and evaluated the proposals for this project.

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